# Influence of directivity pattern order on perceived distance

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# Introduction

The metaphoric idea behind employing the icosahedral loudspeaker array (ICO) in music is to "orchestrate" reflecting surfaces, resulting in the perception of auditory objects at distinct locations in the room [1].

An early study [2] about the perceived direction of auditory objects created by directional sound sources such as the ICO confirms the influence of orientation of directivity on localization deviating from the direct path.

In extension to this preliminary study, this contribution focuses on the perceived distance of auditory objects created by the ICO. The controllability of the perceived distance is examined, which is essential for the application of the ICO as an instrument.

We briefly discuss the method to control the perceived auditory distance using a variable-order directional source and subsequently design a listening experiment based on an auralized room. After this, we discuss results, which are modeled in the last section.

# Controlling the auditory distance

In electro-acoustic music, the notion of adjustabledirectivity loudspeakers was introduced in the late 1980s by researchers at IRCAM. For the renowned concept study "la timée" [3], a cube housing six separately controlled loudspeakers was built to achieve freely controllable directivity. In 2006, researchers at IEM reconsidered the theory and built a larger and more powerful 20sided, 20-channel playback device yielding controllable  $3^{\rm rd}$ -order directivity patterns [4] (see Fig. 1).

Recently Laitinen [5] presented a method to control the perceived distance of an auditory object by changing the directivity pattern of a cubical loudspeaker array.

Directivity control was used to modify the amount of reverberant energy. The direct-to-reverberant energy ratio



Figure 1: Adjustable-directivity loudspeakers "la timée" (left) and ICO (right).



Figure 2: Directivity patterns  $A_{1...4}$  normalized to constant energy.

(D/R-ratio) is known to be a prominent cue for distance perception (see [6] for a thorough review).

The D/R-ratios in numbers does not only depend on the directivity pattern but is essentially shaped by the room response. Still, directivity-pattern designs can be defined that accomplish room-independent control of the auditory distance. Following the idea in [5], the controllability of auditory distance is examined in closer detail here, after allowing a more thorough control of directivity.

Considered directivity patterns are based on frequencyindependent max- $\mathbf{r}_{\rm E}$  beampattern designs, which exhibit a relatively narrow main lobe and permits sufficiently well suppressed side lobes [7]. Seven different directivity patterns were tested, denoted as  $A_{1...7}$ . Table 1 lists these patterns  $A_1 \dots 7$  in particular, and Figure 2 shows the patterns  $A_{1...4}$  (normalized to constant energy).

Table 1: Properties o	f tested o	directivity	patterns.
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- $3^{\rm rd}$  order max- $\mathbf{r}_{\rm E}$  beam towards listener  $A_1$
- $2^{nd}$  order max- $\mathbf{r}_E$  beam towards listener  $A_2$
- $1^{st}$  order max- $\mathbf{r}_{E}$  beam towards listener  $A_3$
- omnidirectional beampattern
- $A_4$
- $1^{st}$  order max- $\mathbf{r}_{E}$  beam away from listener  $A_5$
- $2^{nd}$  order max- $\mathbf{r}_{E}$  beam away from listener  $A_6$
- $3^{\rm rd}$  order max- $\mathbf{r}_{\rm E}$  beam away from listener  $A_7$

# **Experimental Setup**

We investigated the influence of beampatterns on the perceived distance in a listening experiment. The experiment was done at IEM in Graz and is part of a more comprehensive study submitted to DAFx 2016 [8].

Direct sound and early reflections were auralized using the image source method [9], whereas diffuse sound was simulated with the software toolbox MCRoomSim [10].



Figure 3: Setup of the auralized room and sound source using the 24-channel loudspeaker ring.

The auralized room is shoebox shaped  $(10.3 \text{ m} \times 12 \text{ m} \times 4.8 \text{ m})$  with a frequency-independent absorption coefficient of 0.3 and a mean reverberation time of 700 ms. Playback employed a ring of 24 equally-distributed Genelec 8020 loudspeakers with a radius of r = 1.5 m, placed in the anechoic laboratory of the IEM. Figure 3 shows the setup and positioning of the auralized room.

Each listener's task was to indicate the perceived distance on a graphical user interface displaying a continuous slider for each sample in a multi-stimulus set to permit comparative rating along the ordinal scale *very close* (vc), *close* (c), *moderate* (m), *distant* (d), and *very distant* (vd). The subjects were allowed to repeat each sample at will, and sound files were played back in a loop.

During the listening session, the listener was requested to face loudspeaker 1 ( $\phi = 0^{\circ}$ ), which corresponds to the direction of the auralized sound source.

Fifteen listeners participated in the test. All of them were experienced listeners with normal hearing.

### Conditions

To allow comparison, sounds comply with sounds from earlier experiments [2, 5]. We used female speech  $(S_1,$ sample taken from CD  $B \mathcal{C}O$  101, 1992) and Gaussian white noise  $(S_2)$  with signal spectrum and envelope shaped to the speech signal [11, 12]. Both sounds were equalized in level.

The listening test was carried out as a multi-stimulus test in a MUSHRA-like procedure [13]. Each sample represents a directivity pattern and sound.

Both sounds  $S_{1/2}$  were tested with directivities  $A_{1...7}$  in individual sets yielding responses  $x_{1...7}^{I}$  for each subject and sound. To compare results from different sounds,  $A_{1...7}(S_1)$  and  $A_{1...7}(S_2)$ , an additional multi-stimulus set included the selected conditions  $A_{1,4,7}(S_{1,2})$  for both sounds, yielding the responses  $x_{1,4,7}^{I}$  per subject and sound. The responses  $x_{2,3}^{I}$  and  $x_{4,5}^{I}$  were re-mapped for



**Figure 4:** Median and 95% confidence intervals for tested sounds  $S_{1,2}$  and directivity patterns  $A_{1...7}$ .

each listener and sound by linear scaling and shifting to match  $x_{1,4}^{\text{I}}$  with  $x_{1,4}^{\text{II}}$ , and  $x_{4,7}^{\text{I}}$  with  $x_{4,7}^{\text{II}}$ , respectively:

$$x_{i} = \begin{cases} x_{1}^{\mathrm{II}} & \text{for } i \in \{1, 4, 7\}, \\ \frac{x_{4}^{\mathrm{II}} - x_{1}^{\mathrm{II}}}{x_{4}^{\mathrm{II}} - x_{1}^{\mathrm{II}}} (x_{i}^{\mathrm{II}} - x_{1}^{\mathrm{II}}) + x_{1}^{\mathrm{II}} & \text{for } i \in \{2, 3\}, \\ \frac{x_{7}^{\mathrm{II}} - x_{4}^{\mathrm{III}}}{x_{4}^{\mathrm{II}} - x_{1}^{\mathrm{III}}} (x_{i}^{\mathrm{II}} - x_{4}^{\mathrm{IIII}}) + x_{4}^{\mathrm{IIIII}} & \text{for } i \in \{5, 6\}, \end{cases}$$
(1)

i.e., a complete response set  $x_{1...7}$  per listener and sound.

#### Results

Figure 4 shows median values and corresponding 95% confidence intervals of  $x_{1...7}$  using Eq. (1).

For conditions  $A_{1...5}$ , the auditory distance increases monotonically for both sounds. An analysis of variance (ANOVA) of neighboring values reveals conditions  $A_{1...5}$ to be significantly different (p < 0.09). By contrast, conditions  $A_{5...7}$  do not yield a significant change ( $p \ge 0.74$ ). The choice of the sound  $S_1$  or  $S_2$  does not yield a significant difference (p = 0.52), so that the considerations below only uses pooled responses for both sounds  $S_{1,2}$ .

### Modeling the auditory distance

The question is whether the responses can be explained by characteristic metrics used to characterize the spatial sound field in psychoacoustics. Linear regression based on the following simulated metrics were tested:

- Direct-To-Reverberant Energy Ratio,
- Lateral Energy Fraction,
- Inter-aural Cross Correlation Coefficient.

The D/R-ratio is widely accepted for prediction of auditory source distance and hence the most obvious predictor. By contrast, the Lateral Energy Fraction (LF) and Inter-aural Cross Correlation Coefficient (IACC) are both used to describe either listener envelopment or apparent source width [14, 15, 16]. While the D/R and Lateral Energy ratios are positively correlated with features relevant for auditory distance, the IACC is negatively correlated. Regression uses 1–IACC.



Figure 5: Comparison of median and 95% confidence intervals of assessed distance pooled over sounds  $S_{1,2}$  with predictors based on D/R-ratio, LF, and 1–IACC.

Figure 5 compares the median and 95% confidence intervals with the linear regression models for the conditions  $A_{1/7}$ .

All models yield curves that are highly correlated with the experimental data. Interestingly, spatial measures quantyifing the apparent source width turn out almost perfect. This is underlined by their correlations of  $R^2 =$ 0.97 for the LF and  $R^2 = 0.99$  for 1–IACC, whereas the D/R-ratio reaches  $R^2 = 0.93$ .

# Conclusion

We investigated the influence of frequency-independent  $\max - r_E$  directivities on the perceived auditory distance. We could show that for a variable-directivity source pointing its beam towards and away from the listener is able to evoke a series of pronounced and graduated distance impressions.

The mapping of the directivities  $A_{1...7}$  to the perceived distance curve is sigmoid-shaped and thus we could confirm a signal-independent range of controllability.

Finally, we showed that each the D/R-ratio, the LF, and 1–IACC are suitable in linear regression models yielding curves highly correlated to the responses.

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